Environmental Noise Assessment

26, 28, 30, 34, 36, 38, 42 Mill Street and 3 and 11 Dayfoot Drive

Proposed Condominium Development

Mill Street and Dayfoot Drive Georgetown, Halton Hills

> September 7, 2016 Project: 116-0217

> > Prepared for

Amico 42 Mill Ltd

Prepared by

Seema Nagaraj, h.D., P.Eng

Reviewed by

Vic Schroter, Ph.D., P.Ending of Onto



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Environmental Noise Assessment

26, 28, 30, 34, 36, 38, 42 Mill Street and 3 and 11 Dayfoot Drive

Proposed Condominium Development

Mill Street and Dayfoot Drive Georgetown, Halton Hills

EXECUTIVE SUMMARY

Valcoustics Canada Ltd. (VCL) was retained by Amico Properties Inc. to prepare an Environmental Noise Assessment in support of the Site Plan Approval (SPA) application submission to the Town of Halton Hills. The main topic of this assessment addresses the noise impact from the existing environment onto the proposed development; in addition, this assessment addresses the noise impact of the proposed development on adjacent land uses and the noise impact of the proposed development on itself. The proposed project will consist of two 6-storey condominium buildings and one 5-storey retirement residence.

The significant noise sources in the vicinity are rail traffic on the Canadian National Railways (CN) Halton Subdivision north of the proposed development and road traffic on Guelph Street located south of the proposed development.

The sound levels on site have been determined and compared with the applicable Ministry of the Environment and Climate Change (MOE) noise guideline limits to determine the need for noise mitigation.

To meet the applicable transportation noise guideline limits:

- central air conditioning is required for all three buildings;
- windows with Sound Transmission Class (STC) ratings up to 39 are required, depending on exposure to the CN rail line; and
- exterior walls meeting STC 54 are required at all buildings.

The above STC requirements are based on conservative assumptions and may change (be lowered) once more detailed designs are available.

INTRODUCTION 1.0

VCL was retained by Amico Properties Inc. to prepare an Environmental Noise Assessment in support of an SPA application submission to the Town of Halton Hills. The potential sound levels have been predicted and compared to the applicable MOE noise guideline limits. Where sound level excesses above these guideline limits occur, noise mitigation measures have been recommended.

1.1 THE SITE AND SURROUNDING AREA

The site is located at the northwest corner of Guelph Street and Mill Street in Georgetown. The site was previously occupied by the Georgetown Memorial Arena.

The site is bounded by:

- Mill Street, with existing detached residential dwellings beyond, to the east;
- Dayfoot Drive, with existing detached residential dwellings beyond, to the north;
- existing residential development (detached and apartment) to the west; and
- an existing church (Sacre-Coeur Church), with Guelph Street beyond, to the south. The church (Sacre-Coeur Church) is located directly at the northwest corner of Guelph Street and Mill Street.

The CN rail line runs east-west to the north of the site. The closest distance from the rail line to the site is about 100 metres. The Georgetown GO Rail Station is located to the northeast of the site, beyond the existing residential area. The closest distance from the GO station to the site is about 400 metres. The closest distance from the site to the main road traffic corridor (Guelph Street) is about 40 metres.

Small commercial businesses and residences are located on the south side of Guelph Street.

A Key Plan is included as Figure 1.

This report is based on a Masterplan, prepared by Holabird and Root, dated August 23, 2016. The Masterplan is included as Figure 2, which shows the site with the three buildings.

1.2 THE PROPOSED DEVELOPMENT

The development consists of three buildings, constructed in three phases:

- Phase I: Building 1 - 6-storey condominium building on the south side of the site.
- Phase II: Building 2 - 6-storey condominium building on the northwest side of the site.
- Phase III: Building 3 - 5-storey retirement residence on the northeast side of the site.

The conceptual design of the site and the buildings is shown in Figure 2. The entrance to the site will be from Mill Street, with the entrance/access road located between Building 1 and Building 3.

All three buildings are anticipated to have balconies, all less than 4 metres deep. Building 1 will have a ground level outdoor patio area (Outdoor Living Area - "OLA") on the west side of the building. Building 3 will have a ground level OLA on the west side of the building. Building 2 will not be equipped with any OLA's. The locations of the OLA's are shown on Figure 2.

2.0 **ENVIRONMENTAL NOISE ASSESSMENT**

2.1 **NOISE SOURCES**

The noise sources with potential to impact the proposed development are rail traffic on the CN Halton Subdivision north of the proposed development and road traffic on Guelph Street located south of the proposed development. Traffic volumes on the other adjacent roads are considered to be minor and no significant noise impact is expected.

2.1.1 Rail Transportation Sources

2.1.1.1 CN

Rail traffic data for the CN Halton Subdivision applicable to the year 2016 was obtained directly from CN. The CN rail traffic data was escalated to the year 2026 design condition using a growth rate of 2.5% compounded annually. This escalation rate is suggested by the MOE for preparing environmental noise studies.

CN rail activity includes freight and passenger traffic. Current trackage at this point consists of a double mainline track, continuously welded throughout the study area.

2.1.1.2 GO Transit

Commuter rail traffic for the GO Kitchener line, applicable to the year 2025, was obtained directly from GO Transit /Metrolinx. The GO Transit rail traffic data was escalated to the year 2026 design condition using a growth rate of 2.5% compounded annually.

GO Transit rail activity includes commuter trains only.

2.1.2 Road Transportation Sources

For Guelph Street, a turning movement count applicable to the year 2012 was provided by the Town of Halton Hills. It was also assumed that the traffic volumes would approximately follow the typical ITE traffic distribution model. Thus, the 8-hour count is 54.3% of the 24-hour data. The full 24-hour traffic volume was then calculated based on this percentage. A growth rate of 2%, compounded annually, was used to obtain future (year 2026) traffic volumes. Truck percentages were obtained from the turning movement counts. Medium and heavy truck percentages were calculated as 3.8% and 2.8%, respectively, of the total traffic volume. A day/night split of 90%/10% was used as is typical for well travelled roadways.

The road traffic data is summarized in Table 1. Correspondence is included as Appendix A.

2.2 ENVIRONMENTAL NOISE GUIDELINES

2.2.1 MOE Publication NPC-300

The applicable noise guidelines for new residential development are those in MOE Publication NPC-300, "Environmental Noise Guideline, Stationary and Transportation Sources – Approval and Planning". These noise guidelines are discussed briefly below and summarized in Appendix B.

2.2.1.1 Architectural Elements

In the daytime (0700 hours to 2300 hours), the indoor criterion for road noise is $L_{eq\,Day}^{(1)}$ of 45 dBA for sensitive spaces such as living/dining rooms, dens and bedrooms. At night, the indoor criterion for road noise is $L_{eq\,Night}^{(2)}$ of 45 dBA for sensitive spaces such as living/dining rooms and dens and 40 dBA for bedrooms. The indoor criteria for rail noise are 5 dBA more stringent than those for road; that is, 40 dBA for living/dining rooms and dens during the daytime and nighttime periods, 40 dBA for bedrooms during the daytime period and 35 dBA for bedrooms during the nighttime period.

The architectural design of the building envelope (walls, windows, etc.) must provide adequate sound isolation to achieve these indoor sound level limits, based on the applicable outdoor sound level on the facades.

2.2.1.2 Ventilation

In accordance with the MOE noise guidelines for road traffic sources, if the daytime sound level, $L_{eq\;Day}$, at the exterior face of a noise sensitive window is greater than 65 dBA, means must be provided so that windows can be kept closed for noise control purposes and central air conditioning is required. For daytime sound levels between 56 dBA and 65 dBA inclusive, there need only be the provision for adding air conditioning at a later date. A warning clause advising the occupant of the potential interference with some activities is also required. At nighttime, air conditioning would be required when the sound level exceeds 60 dBA ($L_{eq\;Night}$) at a noise sensitive window (provision for adding air conditioning is required when greater than 50 dBA).

2.2.1.3 Outdoors

For OLA's, the guideline is $L_{eq\ Day}$ of 55 dBA, with an excess not exceeding 5 dBA considered acceptable if it is technically not practicable to achieve the 55 dBA objective, providing warning clauses are registered on title. Note that for road traffic sources, a balcony is not considered an OLA, unless it is the only OLA for the occupant and it is:

- at least 4 m in depth; and
- unenclosed.
- (1) $L_{eq Day}$: 16-hour energy equivalent sound level (0700-2300 hours).
- (2) L_{eq Night}: 8-hour energy equivalent sound level (2300-0700 hours).

2.2.2 Halton Region

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The proposed development is not immediately adjacent to any Regional Roads. Thus, there are no regional requirements over and above those of the MOE that apply.

2.2.3 Federation of Canadian Municipalities (FCM) and Railway Association of Canada (RAC)

The standard mitigation requirements outlined in the FCM/RAC guidelines suggest a dwelling setback of 30 m for a residential development adjacent to a principal main line, if in combination with a safety berm at least 2.5 m above the property line grade. A 5.5 m high sound barrier is also suggested (e.g., 3.0 m high acoustic fence atop 2.5 m high safety berm).

Note that the site is well beyond the 30 m setback. In addition, there is existing residential development between the subject site and the rail line. Thus, the safety berm requirements are not applicable in this case.

Warning clauses are also recommended.

Aside from "standard" requirements regarding the setback of dwellings and safety berm/sound barrier configuration, the sound level design objectives of FCM/RAC are similar to those of the MOE.

2.3 NOISE IMPACT ASSESSMENT

Using the road traffic data in Table 1A and rail traffic data in Table 1B, the sound levels in terms of $L_{\text{eq Day}}$ and $L_{\text{eq Night}}$ were determined using STAMSON V5.04 – ORNAMENT, the computerized road traffic noise prediction models of the MOE.

In calculating the sound levels at the facades, the calculations were performed at the highest storeys (worst case) and at anticipated window locations. The daytime OLA sound levels were calculated in the two OLA's at Buildings 1 and 3. The calculation was performed at the centre of the OLA, at a height of 1.5 m above grade. Inherent screening of each building face due to its orientation to the noise source as well as that provided by the subject development itself were taken into account.

Note that the development will be built in three phases. Screening from the previous phases, but not the future phases, was included in the sound level assessments at each building.

The surrounding residential developments are primarily low-rise, with the exception of the apartment building to the west of the site. To be conservative, screening from the neighbouring developments were not included in the assessment of the sound levels at the building facades. Since both of the OLA's are at grade level, it is anticipated that there would be a significant amount of screening from the neighbouring developments. Thus, screening from the surrounding developments was included in the OLA sound level assessment.

Tables 2-1, 2-2 and 2-3 summarize the predicted sound levels outdoors at specific locations.

A sample sound level calculation is included in Appendix C.

The highest daytime/nighttime sound levels would occur in the northwest corners of each building, with highest sound levels of 63 dBA/65 dBA at the north west corner of Building 2. The highest daytime OLA sound level is 52 dBA.

3.0 NOISE ABATEMENT REQUIREMENTS

In general, the noise control measures can be classified into two categories:

- Architectural elements to achieve acceptable indoor noise guidelines for (a) transportation sources: and
- (b) Design features to protect the OLA's.

Noise abatement requirements are summarized in Table 3 and notes to Table 3.

3.1 **INDOORS**

3.1.1 Architectural Requirements

The indoor noise level guidelines for the transportation sources can be achieved by using appropriate construction for exterior walls, windows and doors. In determining the worst-case architectural requirements for the dwellings, wall and window areas were assumed to be 20% and 80%, respectively, of the associated floor area, on the facades directly exposed to and at an angle to the noise sources, for both living/dining rooms and bedrooms.

For all three buildings (residential units) in this development, the STC requirements depend on the location and orientation of the exterior walls and windows. The exterior walls are required to meet a minimum STC value of 54. In order to meet the MOE criteria, the most onerous requirements for the windows is a minimum STC value of 39. See Table 3 for details.

The above STC requirements are based on conservative assumptions and may change (be lowered) once more detailed designs are available.

3.1.2 Ventilation Requirements

Based on the predicted daytime and nighttime sound levels, all three buildings (residential units) in this development will be required to include central air conditioning.

3.2 **OUTDOORS**

There are two ground level outdoor amenity areas that were considered and assessed as OLA's. The first OLA is located at the southwest facade of Building 1 and the second is located on the west side of the Retirement Residence (Building 3). The unmitigated daytime OLA sound levels are within the 55 dBA design guideline. Thus, no sound barriers or other mitigation is required for noise control purposes.

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3.3 **WARNING CLAUSES**

Where the sound level guidelines are exceeded, appropriate MOE warning clauses should be registered on title and make future occupants aware of the potential noise situation. Locations requiring warning clauses and the appropriate wording are given in Table 3 and in notes to Table 3. respectively.

4.0 THE EFFECT OF THE PROJECT ON THE NEIGHBOURHOOD

The main source of noise associated with potential noise impact of this development on surrounding uses/receptors is the mechanical equipment.

Mechanical equipment interfacing to the outdoors is required to comply with the MOE noise guideline limits in NPC-300. By proper engineering design, all requirements can be met and no adverse noise impact would be created for surrounding uses. Appropriate choice of location, equipment type, and noise control features should be considered during detailed design for such items as rooftop equipment and air intakes and exhausts, including underground parking garage ventilation systems. Any parking garage air shafts located immediately adjacent to residential uses, in addition to appropriate choice of fan type, may need special noise control treatment such as acoustically lining the shaft or providing silencers.

For any emergency generators, appropriate steps should be taken to ensure that the equipment placement, treatment, and the routine testing schedule will not generate adverse noise impact on neighbouring properties. For generators under 700 kW, the installation must comply with Ontario Regulation 346/12.

The additional road traffic generated by this project will be small relative to existing traffic volumes within the general area, and is not expected to create adverse noise impact.

5.0 THE EFFECT OF THE PROJECT ON ITSELF

Same as above, the main source of noise associated with potential noise impact of each of the three buildings on the other buildings in this development is the mechanical equipment. The same requirements described above in Section 4.0 apply.

Consideration should be given to the control of airborne and/or structure-borne noise generated within each building as part of the detailed design. The major items requiring attention are the common boundaries and building services.

The common boundaries, in general, are those between adjacent noise sensitive areas (such as two adjacent residential units) and between noise sensitive areas and noisy service areas (such as a residential unit and a mechanical space). Building services include mechanical equipment, plumbing, etc.

6.0 CONCLUSIONS

With the incorporation of the recommended noise mitigation measures, the applicable MOE noise guidelines can be met and a suitable acoustical environment provided for the occupants.

To meet the applicable transportation noise guideline limits, the three buildings require central air conditioning, windows with STC ratings up to 39 and exterior walls meeting STC 54. The STC requirements are based on conservative assumptions and may change (be lowered) when detailed designs become available.

7.0 REFERENCES

- 1. PC STAMSON 5.04, "Computer Program for Road Traffic Noise Assessment", Ontario Ministry of the Environment.
- 2. Building Practice Note No. 56: "Controlling Sound Transmission into Buildings", by J. D. Quirt, Division of Building Research, National Council of Canada, September 1985.
- 3. Environmental Noise Guideline Stationary and Transportation Sources, Approval and Planning", Ontario Ministry of the Environment, Publication NPC-300, October 2013.
- 4. "Guideline for New Development in Proximity to Railway Operations", Federation of Canadian Municipalities and the Railway Association of Canada, May 2013.

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TABLE 1A

ROAD TRAFFIC DATA

Deadway	V	AADT ⁽¹⁾	% Trucks		Day/Night	Speed
Roadway	Year		Medium	Heavy	(%)	Limit (kph)
Guelph Street (2)	2012	24 275	3.8	2.8	90/10	50

Notes:

(1) AADT – Annual Average Daily Traffic.

(2) Obtained from the Town of Halton Hills for the year of 2012. Future (year 2026) traffic volumes were obtained by projecting the current (year 2012) traffic data at a growth rate of 2%, compounded annually. Truck percentages were calculated from the turning movement count data. Day/night split was assumed.

TABLE 1B

RAIL TRAFFIC DATA – CN HALTON SUBDIVISION

Period	Train Type	Maximum # of Trains	Maximum # of Cars/Train	Max # of Locos/Train	Maximum Speed (kph)
	Freight ⁽¹⁾	10 (12.8) ⁽³⁾	140	4	80
Daytime (0700 to 2300)	Passenger ⁽¹⁾	4 (5.1) ⁽³⁾	10	2	80
	GO Commuter ⁽²⁾	7 (7.2)(3)	12	1	80
	Freight ⁽¹⁾	8 (10.2) ⁽³⁾	140	4	80
Nighttime (2300 to 0700)	Passenger ⁽¹⁾	0 (0)(3)	10	2	80
,	GO Commuter ⁽²⁾	5 (5.1) ⁽³⁾	12	1	80

Notes:

(1) Obtained directly from CN for the year 2016.

(2) Obtained directly from GO Transit for the year 2025. (3) The data shown in brackets is projected to the year 2

The data shown in brackets is projected to the year 2026 with a 2.5% growth rate, compounded annually.

TABLE 2A

BUILDING 1

PREDICTED UNMITIGATED SOUND LEVELS OUTDOORS(1)

Location ⁽²⁾	Source	Distance (m) ⁽³⁾	L _{eq Day} (dBA) ⁽¹⁾	L _{eq Night} (dBA) ⁽¹⁾
	Guelph Street	106	47	_
OLA	CN Halton Subdivision	261	51	_
	TOTAL	-	52	-
	Guelph Street	95	59	52
Southwest Corner (South Face)	CN Halton Subdivision	206	56	58
(1111	TOTAL	-	61	59
	Guelph Street	95	54	47
Southwest Corner (West Face)	CN Halton Subdivision	206	61	63
(TOTAL	-	62	63
	Guelph Street	117	53	46
Northwest Corner (West Face)	CN Halton Subdivision	190	61	63
,	TOTAL	-	62	63
Northwest Corner (North Face)	CN Halton Subdivision	190	61	63
	Guelph Street	59	61	55
Southeast Corner (South Face)	CN Halton Subdivision	261	55	57
(333 333)	TOTAL	_	62	59
Southeast Corner (East Face)	Guelph Street	59	61	54

Notes:

At Buildings 1 and 2, daytime/nighttime receptors at the building facades were taken at a height of 16.5 m above grade, (1) representing the sixth (top) floor windows. At Building 3, daytime/nighttime receptors at the building facades were taken at a height of 13.5 m above grade, representing the fifth (top) floor windows. OLA receptors were taken at 1.5 m above grade. See Figure 2 for receptor locations.

⁽²⁾ (3)

Distance indicated is from the centreline of the noise sources to facade or OLA.

TABLE 2B BUILDING 2 PREDICTED UNMITIGATED SOUND LEVELS OUTDOORS(1)

Location ⁽²⁾	Source	Distance (m) ⁽³⁾	L _{eq Day} (dBA) ⁽¹⁾	L _{eq Night} (dBA) ⁽¹⁾
	Guelph Street	138	52	45
Southwest Corner (South Face)	CN Halton Subdivision	174	57	59
,	TOTAL	ı	58	59
	Guelph Street	138	52	45
Southwest Corner (West Face)	CN Halton Subdivision	174	62	64
(TOTAL	_	62	64
	Guelph Street	186	50	44
Northwest Corner (West Face)	CN Halton Subdivision	141	63	65
,	TOTAL	ı	63	65
Northwest Corner (North Face)	CN Halton Subdivision	141	62	64
Southeast Corner (East Face)	Guelph Street	126	53	46

Notes:

⁽¹⁾ At Buildings 1 and 2, daytime/nighttime receptors at the building facades were taken at a height of 16.5 m above grade, representing the sixth (top) floor windows. At Building 3, daytime/nighttime receptors at the building facades were taken at a height of 13.5 m above grade, representing the fifth (top) floor windows. OLA receptors were taken at 1.5 m above grade. See Figure 2 for receptor locations.

⁽²⁾ (3) Distance indicated is from the centreline of the noise sources to facade or OLA.

TABLE 2C

BUILDING 3

PREDICTED UNMITIGATED SOUND LEVELS OUTDOORS(1)

Location ⁽²⁾	Source	Distance (m) ⁽³⁾	L _{eq Day} (dBA) ⁽¹⁾	L _{eq Night} (dBA) ⁽¹⁾
OLA	CN Halton Subdivision	180	46	_
	Guelph Street	123	51	44
Southwest Corner (South Face)	CN Halton Subdivision	200	51	52
(3.2.2.)	TOTAL	1	54	53
Northwest Corner (West Face)	Guelph Street	171	60	62
Northwest Corner (North Face)	CN Halton Subdivision	171	60	62
Southeast Corner (East Face)	Guelph Street	100	57	50

Notes:

At Buildings 1 and 2, daytime/nighttime receptors at the building facades were taken at a height of 16.5 m above grade, representing the sixth (top) floor windows. At Building 3, daytime/nighttime receptors at the building facades were taken at a height of 13.5 m above grade, representing the fifth (top) floor windows. OLA receptors were taken at 1.5 m above grade. See Figure 2 for receptor locations. (1)

⁽²⁾ (3) Distance indicated is from the centreline of the noise sources to facade or OLA.

TABLE 3 **MINIMUM NOISE ABATEMENT MEASURES**

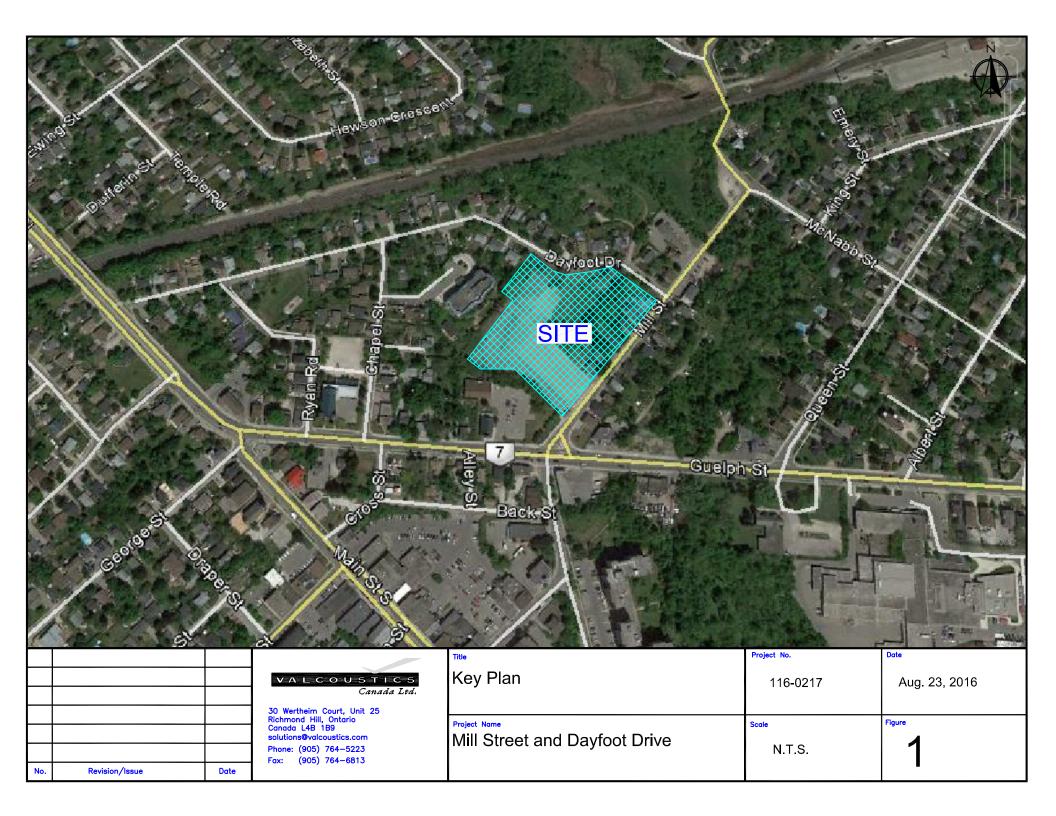
Location	Air Conditioning ⁽¹⁾	Exterior Wall STC Rating ⁽²⁾	Window STC Rating ⁽³⁾	Warning Clauses ⁽⁴⁾
Phase 1 Condominium Building (North and West Facade)	Mandatory	STC 54	STC 37	A + B + C
Phase 1 Condominium Building (South and East Facade)	Mandatory	STC 54	STC 33	A + B + C
Phase 2 Condominium Building (West Facade)	Mandatory	STC 54	STC 39	A + B + C
Phase 2 Condominium Building (North Facade)	Mandatory	STC 54	STC 38	A + B + C
Phase 2 Condominium Building (South and West facade)	Mandatory	STC 54	STC 33	A + B + C
Phase 3 Retirement Residence (North and West facade)	Mandatory	STC 54	STC 37	A + B + C
Phase 3 Retirement Residence (South and East Facade)	Mandatory	STC 54	STC 30	A + B + C
OLA - Building 1	No abatement measures are required			
OLA - Building 3	No abatement measures are required			

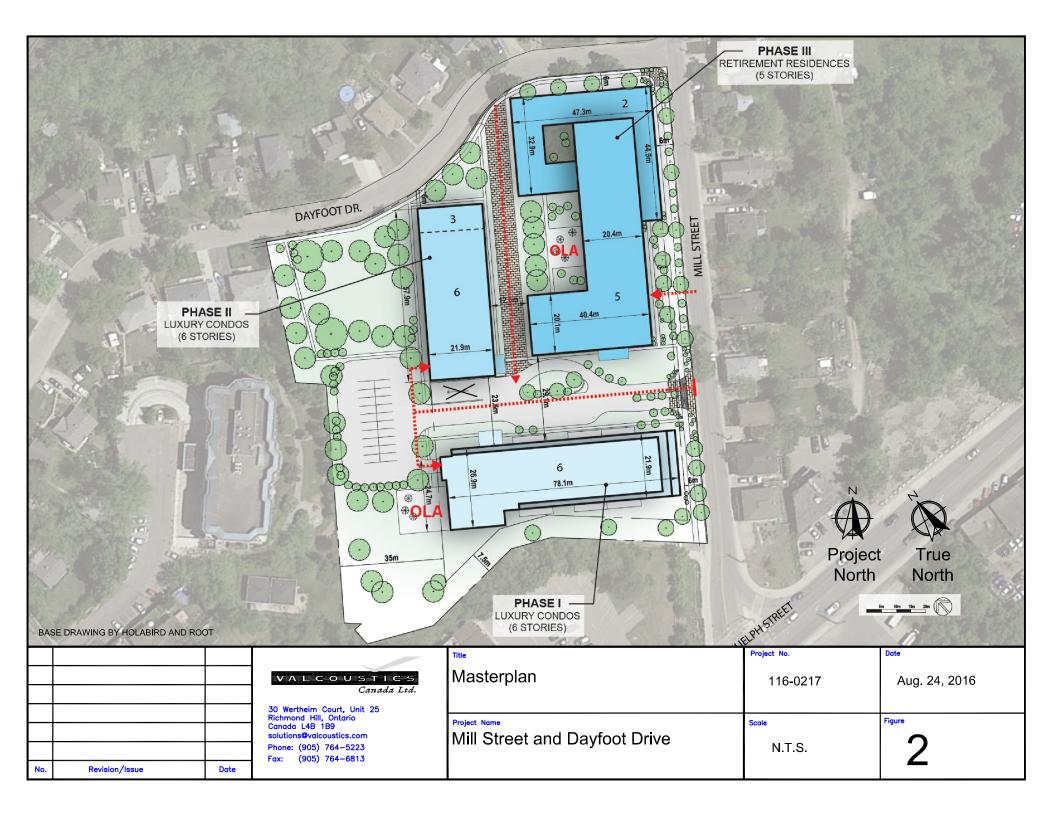
For notes to this table, see following page.

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NOTES TO TABLE 3

- (1) Air conditioning means central air conditioning either for the building as a whole or for individual units.
- (2) STC Sound Transmission Class Rating (Reference ASTM-E413).
 - The requirements are based on assumed wall to associated indoor floor areas (20% wall to floor area and 80% window to floor area for living rooms/bedrooms). The requirements should be confirmed when building plans are available.
- (3) A sliding glass walkout door should be considered as a window and be included in the percentage of glazing.
 - The requirements are based on assumed window to associated indoor floor area (20% wall to floor area and 80% window to floor area). The requirements should be confirmed when building plans are available.
- (4) Warning clauses to be registered on title and be included in Offers of Purchase and Sale and Leases on designated units:
 - A. "Purchasers and tenants/lessees are advised that despite the inclusion of noise control features in this development and within the building units, sound levels due to increasing road traffic may on occasion interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and Ministry of the Environment."
 - B. "This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."
 - C. "Canadian National Railways or its affiliated railway companies has or have a railway right-of-way within 300 m from this dwelling unit. There may be alterations to or expansions of the railway facilities of such right-of-way in the future, including the possibility that Canadian National Railways or its affiliated railway companies as aforesaid, or their assigns or successors may expand their business operations. Such expansion may affect the living and business environment of the residents, tenants and their visitors, employees, customers and patients in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating features in the design of the development. Canadian National Railways, its affiliated railway companies and their successors and assigns will not be responsible for any complaints or claims arising from use of such facilities and/or operations on, over or under the aforesaid right-of-way."
- (5) Conventional roof construction meeting Ontario Building Code requirements is satisfactory in all cases.
- (6) All exterior doors shall be fully weatherstripped.





APPENDIX A ROAD AND RAIL TRAFFIC DATA

Seema Nagaraj

From: Brandon Gaffoor <Brandon.Gaffoor@gotransit.com>

Sent: July-21-16 2:21 PM **To:** Seema Nagaraj

Cc: Vic Schroter; Adam Snow

Subject: RE: Rail traffic data request (VCL File: 116-0217)

Hello Seema.

Sorry for the delay in our response,

Further to your request of May 31, 2016, It's anticipated that GO Service on the adjacent Kitchener Line will be comprised of diesel trains within (at least) a 10 year time horizon. The preliminary midterm (2025) weekday train volume forecast at this location, including both revenue and equipment trips, is in the order of 12 trains (Diesel: 7 Day, 5 Night). Trains will be comprised of a single locomotive and up to 12 passenger cars.

The maximum design speed on the Kitchener line, adjacent to the subject site, is 80 kph (50 mph). Bells and whistles will be used as per standard protocol at Georgetown Station.

This information is subject to change and may be influenced by, among other factors, service planning priorities, operational considerations, funding availability and passenger demand.

It should be noted that VIA and CN operate trains in this area – as such it would be prudent to contact those organizations directly for rail traffic information.

I trust that this information is useful. Please feel free to contact me should you have any additional questions.

Kind Regards,

Brandon Gaffoor

Co-op Student | Rail Corridor Management Office | Rail Corridors Metrolinx | 335 Judson Street | Toronto | Ontario | M8Z 1B2

□ | Brandon.Gaffoor@GoTransit.com

2 | 416.202.0118







From: Seema Nagaraj
Sent: May-31-16 5:02 PM
To: Adam.Snow@gotransit.com

Subject: Rail traffic data request (VCL File: 116-0217)

Hi Adam,

We are currently preparing an environmental noise study in the area of Mill Street and Dayfoot Drive in Georgetown (see attached image for location). We are looking for GO rail data for the CN Halton Subdivision east of Main Street North.

Please provide:

Future day/night train volumes
Number of locomotives per train
Number of cars per train
Speed
Whistle blowing locations (at grade crossing)

Thank you,

Seema Nagaraj, Ph.D., EIT



30 Wertheim Court, Unit 25 Richmond Hill, Ontario Canada L4B 1B9 Tel: 905-764-5223 ext. 243 Fax: 905-764-6813 solutions@valcoustics.com

This e-mail is intended only for the person or entity to which it is addressed. If you received this in error, please contact the sender and delete all copies of the e-mail together with any attachments.

Project Number: HAL - 23.64 - McNabb Street, Georgetown, ON

Dear Seema:

Date: 2016/06/13

Re: Train Traffic Data – CN Halton Subdivision near McNabb Street in Georgetown, ON

The following is provided in response to Seema's 2016/05/31 request for information regarding rail traffic in the vicinity of McNabb Street in Orangeville at approximately Mile 23.64 on CN's Halton Subdivision.

Typical daily traffic volumes are recorded below. However, traffic volumes may fluctuate due to overall economic conditions, varying traffic demands, weather conditions, track maintenance programs, statutory holidays and traffic detours that when required may be heavy although temporary. For the purpose of noise and vibration reports, train volumes must be escalated by 2.5% per annum for a 10-year period.

Typical daily traffic volumes at this site location are as follows:

*Maximum train speed is given in Miles per Hour

	0700-2300	e Brande e Brande e e e e e e e e e e e e e e e e e e	a transfer of the second of th	
Type of Train	Volumes	Max.Consist	Max. Speed	Max. Power
Freight	10	140	50	4
Way Freight	******	25	50	4
Passenger	4	10	50	2

	2300-0700			
Type of Train	Volumes	Max.Consist	Max. Speed	Max. Power
Freight	8	140	50	4
Way Freight	0	25	50	4
Passenger	0	10	50	2

The volumes recorded reflect westbound and eastbound freight and passenger operations on CN's Halton Subdivision.

Except where anti-whistling bylaws are in effect, engine-warning whistles and bells are normally sounded at all at-grade crossings. There are zero at-grade crossing in the immediate vicinity of the study area. Anti-whistling bylaws are not in effect at this crossing. Please note that engine warning whistles may be sounded in cases of emergency, as a safety and or warning precaution at station locations and pedestrian crossings and occasionally for operating requirements.

With respect to equipment restrictions, the gross weight of the heaviest permissible car is 286,000 lbs.

The double mainline track is considered to be continuously welded rail throughout the study area. The presence of one switch located at Mile 23.78 may exacerbate the noise and vibration caused by train movements.

The Canadian National Railway continues to be strongly opposed to locating developments near railway facilities and rights-of-way due to potential safety and

environmental conflicts. Development adjacent to the Railway Right-of-Way is not appropriate without sound impact mitigation measures to reduce the incompatibility. For confirmation of the applicable rail noise, vibration and safety standards, Mr. Raymond Beshro, Canadian National Railway Properties at 514-399-7627 should be contacted directly.

I trust the above information will satisfy your current request.

Sincerely,

Derek Basso

Engineering Technician

Derek.Basso@cn.ca

Duch Busso

cc. Raymond Beshro - CN - via e-mail

Guelph St @ Maple Ave **Morning Peak Diagram Specified Period One Hour Peak** From: 8:00:00 From: 7:00:00 To: 9:00:00 To: 9:00:00 Municipality: Halton Hills Weather conditions: Rain am, Cloudy/Dry mid+pm Site #: 000000004 Guelph St & Maple Ave Person(s) who counted: Intersection: Bolek TFR File #: Sophie Count date: 17-Dec-2012 ** Signalized Intersection ** Major Road: Guelph St runs W/E North Leg Total: 741 Heavys 14 1 24 Heavys 25 East Leg Total: 2108 16 North Entering: 323 Trucks 7 1 Trucks 25 East Entering: 852 North Peds: 24 Cars 45 192 46 283 Cars 368 East Peds: 18 \mathbb{X} Peds Cross: Totals 66 209 Totals 418 Peds Cross: ⋈ 48 Maple Ave Totals Heavys Trucks Cars Trucks Heavys Totals Cars 28 42 547 617 79 2 7 88 470 424 32 14 277 10 294 Guelph St 780 31 Heavys Trucks Cars Totals Guelph St 10 84 106 12 12 33 764 809 Trucks Heavys Totals 5 39 47 3 Cars 27 48 887 1185 50 1256 Maple Ave \mathbb{X} Peds Cross: Peds Cross: \bowtie Cars 508 Cars 78 205 375 658 West Peds: 30 Trucks 20 Trucks 3 13 32 South Peds: 35 16 West Entering: 962 Heavys 22 Heavys 0 8 14 South Entering: 704 West Leg Total: 1579 Totals 81 South Leg Total: 1254 Totals 550 399 **Comments**

Guelph St @ Maple Ave Mid-day Peak Diagram **Specified Period One Hour Peak** From: 11:00:00 **From:** 11:45:00 To: 14:00:00 To: 12:45:00 Municipality: Halton Hills Weather conditions: Rain am, Cloudy/Dry mid+pm Site #: 000000004 Guelph St & Maple Ave Person(s) who counted: Intersection: Bolek TFR File #: Sophie Count date: 17-Dec-2012 ** Signalized Intersection ** Major Road: Guelph St runs W/E North Leg Total: 456 Heavys 10 0 16 Heavys 27 East Leg Total: 1872 2 12 North Entering: 238 Trucks 4 Trucks 9 East Entering: 894 North Peds: 66 Cars 58 122 30 210 Cars 182 East Peds: 22 \mathbb{Z} Totals 72 Totals 218 Peds Cross: 134 32 Peds Cross: Maple Ave Totals Trucks Heavys Totals Heavys Trucks Cars Cars 24 29 656 709 30 1 3 34 576 24 10 610 239 1 250 10 Guelph St 845 35 14 Heavys Trucks Cars Totals Guelph St 4 49 72 19 14 23 607 644 Trucks Heavys Totals 2 32 35 1 Cars 34 29 688 924 36 18 978 Maple Ave \mathbb{X} Peds Cross: Peds Cross: \bowtie Cars 393 Cars 22 103 287 412 West Peds: 69 Trucks 18 Trucks 1 4 11 16 South Peds: 136 West Entering: 751 Heavys 8 Heavys 4 5 4 13 South Entering: 441 West Leg Total: 1460 Totals 27 South Leg Total: 860 Totals 419 **Comments**

Guelph St @ Maple Ave **Afternoon Peak Diagram Specified Period One Hour Peak** From: 15:00:00 **From:** 15:15:00 To: 18:00:00 To: 16:15:00 Municipality: Halton Hills Weather conditions: Rain am, Cloudy/Dry mid+pm Site #: 000000004 Guelph St & Maple Ave Person(s) who counted: Intersection: Bolek TFR File #: Sophie Count date: 17-Dec-2012 ** Signalized Intersection ** Major Road: Guelph St runs W/E North Leg Total: 702 Heavys 1 3 10 Heavys 15 East Leg Total: 3060 14 Trucks 5 7 2 East Entering: North Entering: 384 Trucks 10 1753 North Peds: East Peds: Cars 78 224 58 360 Cars 293 22 \mathbb{Z} Totals 318 Peds Cross: Totals 84 237 Peds Cross: \bowtie 63 Maple Ave Trucks Heavys Totals Heavys Trucks Cars Totals Cars 22 36 1175 1233 0 0 24 1012 27 15 1054 653 8 675 14 Guelph St 1689 23 Heavys Trucks Cars Totals Guelph St 9 5 59 73 31 30 736 797 Trucks Heavys Totals 5 59 70 6 Cars 45 854 1234 35 38 1307 Maple Ave \mathbb{X} Peds Cross: Peds Cross: \bowtie Cars 936 Cars 85 210 440 735 West Peds: 32 Trucks 27 Trucks 4 5 3 12 South Peds: 99 West Entering: 940 Heavys 6 4 16 South Entering: 763 Heavys 19 West Leg Total: 2173 Totals 95 South Leg Total: 1745 Totals 982 **Comments**

Guelph St @ Maple Ave

Total Count Diagram

Municipality: Halton Hills
Site #: 0000000004

Intersection: Guelph St & Maple Ave

TFR File #: 9

North Leg Total: 4816

North Entering: 2330

North Peds:

Peds Cross:

Count date: 17-Dec-2012

Weather conditions:

Rain am, Cloudy/Dry mid+pm

Person(s) who counted:

Major Road: Guelph St runs W/E

Bolek Sophie

** Signalized Intersection **

223

⋈

Heavys 58 50 12 120 Trucks 43 53 19 115

Cars 425 1368 302
Totals 526 1471 333

Heavys 132
Trucks 95
Cars 2259
Totals 2486

East Leg Total: 17041
East Entering: 8486
East Peds: 96
Peds Cross: \$\mathbb{X}\$

Heavys Trucks Cars Totals 171 241 6052 6464



Guelph St

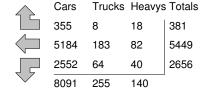
Heavys	Trucks	Cars	Totals
72	41	554 5403	667
113	194	5403	5710
14	25	301	340
199	260	6258	





2095

Maple Ave



272

Guelph St

8118

Maple Ave

			,
Cars	Trucks	Heavys	Totals

Peds Cross:

West Peds: 405

West Entering: 6717

West Leg Total: 13181

Cars 4221
Trucks 142
Heavys 104
Totals 4467



 Cars
 443
 1350
 2413
 4206

 Trucks
 15
 46
 59
 120

 Heavys
 31
 42
 40
 113

 Totals
 489
 1438
 2512

Peds Cross:
South Peds: 545

South Entering: 4439

South Leg Total: 8906

8555

Comments

APPENDIX B

SUMMARY OF MOE NOISE GUIDELINES NPC-300

APPENDIX B

ENVIRONMENTAL NOISE GUIDELINES

MINISTRY OF THE ENVIRONMENT AND CLIMATE CHANGE (MOE)

MOE Publication NPC-300, October 2013: "Environmental Noise Guideline, Reference: Stationary and Transportation Source – Approval and Planning".

SPACE	SOURCE	TIME PERIOD	CRITERION
Living/dining, den areas of residences, hospitals, nursing homes, schools, daycare centres, etc.	Road Rail Aircraft	07:00 to 23:00 07:00 to 23:00 24-hour period	45 dBA 40 dBA NEF/NEP 5
Living/dining, den areas of residences, hospitals, nursing homes, etc. (except schools or daycare centres)	Road Rail Aircraft	23:00 to 07:00 23:00 to 07:00 24-hour period	45 dBA 40 dBA NEF/NEP 5
Sleeping quarters	Road Rail Aircraft	07:00 to 23:00 07:00 to 23:00 24-hour period	45 dBA 40 dBA NEF/NEP 0
Sleeping quarters	Road Rail Aircraft	23:00 to 07:00 23:00 to 07:00 24-hour period	40 dBA 35 dBA NEF/NEP 0
Outdoor Living Areas	Road and Rail	07:00 to 23:00	55 dBA
Outdoor Point of Reception	Aircraft	24-hour period	NEF/NEP 30#
	Stationary Source Class 1 Area	07:00 to 19:00 ⁽¹⁾ 19:00 to 23:00 ⁽¹⁾	50 [*] dBA 50 [*] dBA
	Class 2 Area	07:00 to 19:00 ⁽²⁾ 19:00 to 23:00 ⁽²⁾	50 [*] dBA 45 [*] dBA
	Class 3 Area	07:00 to 19:00 ⁽³⁾ 19:00 to 23:00 ⁽³⁾	45 [*] dBA 40 [*] dBA
	Class 4 Area	07:00 to 19:00 ⁽⁴⁾ 19:00 to 23:00 ⁽⁴⁾	55 [*] dBA 55 [*] dBA

..../cont'd

SPACE	SOURCE	TIME PERIOD	CRITERION
Plane of a Window of Noise Sensitive Spaces	Stationary Source Class 1 Area	07:00 to 19:00 ⁽¹⁾ 19:00 to 23:00 ⁽¹⁾ 23:00 to 07:00 ⁽¹⁾	50° dBA 50° dBA 45° dBA
	Class 2 Area	07:00 to 07:00 ⁽²⁾ 19:00 to 23:00 ⁽²⁾ 23:00 to 07:00 ⁽²⁾	50 [*] dBA 50 [*] dBA 45 [*] dBA
	Class 3 Area	07:00 to 19:00 ⁽³⁾ 19:00 to 23:00 ⁽³⁾ 23:00 to 07:00 ⁽³⁾	45 [*] dBA 45 [*] dBA 40 [*] dBA
	Class 4 Area	07:00 to 19:00 ⁽⁴⁾ 19:00 to 23:00 ⁽⁴⁾ 23:00 to 07:00 ⁽⁴⁾	60° dBA 60° dBA 55° dBA

may not apply to in-fill or re-development.

MOE Publication ISBN 0-7729-2804-5, 1987: "Environmental Noise Reference: Assessment in Land-Use Planning".

EXCESS ABOVE RECOMMENDED SOUND LEVEL LIMITS (dBA)	CHANGE IN SUBJECTIVE LOUDNESS ABOVE	MAGNITUDE OF THE NOISE PROBLEM	NOISE CONTROL MEASURES (OR ACTION TO BE TAKEN)
No excess (<55 dBA)	_	No expected noise problem	None
1 to 5 inclusive (56 to 60 dBA)	Noticeably louder	Slight noise impact	If no physical measures are taken, then prospective purchasers or tenants should be made aware by suitable warning clauses.
6 to 10 inclusive (61 - 65 dBA)	Almost twice as loud	Definite noise impact	Recommended.
11 to 15 inclusive (66 - 70 dBA)	Almost three times as loud	Serious noise impact	Strongly Recommended.
16 and over (>70 dBA)	Almost four times as loud	Very serious noise impact	Strongly Recommended (may be mandatory).

or the minimum hourly background sound exposure $L_{\rm eq}(1)$, due to road traffic, if higher.

Class 1 Area: Urban

Class 2 Area: Urban during day; rural-like evening and night

Class 3 Area: Rural

⁽²⁾ (3) (4) Class 4 Area: Subject to land use planning authority's approval

APPENDIX C

SAMPLE SOUND LEVEL CALCULATION

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STAMSON 5.04 NORMAL REPORT Date: 23-08-2016 09:52:49 MINISTRY OF THE ENVIRONMENT AND CLIMATE CHANGE / NOISE ASSESSMENT
Filename: p2 nw wf.te
                                        Time Period: Day/Night 16/8 hours
Description: Building 2 - West Facade
Rail data, segment # 1: CN Halton (day/night)
             ! Trains ! Speed !# loc !# Cars! Eng !Cont
! (km/h) !/Train!/Train! type !weld
Type
* 1. Freight ! 12.8/10.2 ! 80.0 ! 4.0 !140.0 !Diesel! Yes 2. Passenger ! 5.1/0.0 ! 80.0 ! 2.0 ! 10.0 !Diesel! Yes * 3. GO Commuter ! 7.2/5.1 ! 80.0 ! 1.0 ! 12.0 !Diesel! Yes * The identified number of trains have been adjusted for future growth using the following parameters:
Train type: ! Unadj. ! Annual % ! Years of !
No Name ! Trains ! Increase ! Growth !

1. Freight ! 10.0/8.0 ! 2.50 ! 10.00 !
3. GO Commuter ! 7.0/5.0 ! 2.50 ! 1.00 !
Data for Segment # 1: CN Halton (day/night)
Angle1 Angle2 : -90.00 deg 55.00 deg Wood depth : 0 (No woods
                                                   (No woods.)
Wood depth : 0
No of house rows : 0 / 0
Surface : 1
                                                    (Absorptive ground surface)
Receiver source distance : 141.00 / 141.00 m

Receiver height : 16.50 / 16.50 m

Topography : 1 (Flat/gentle slope; no barrier)
No Whistle
                          : 0.00
Reference angle
Results segment # 1: CN Halton (day)
LOCOMOTIVE (0.00 + 62.29 + 0.00) = 62.29 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
   -90 55 0.14 74.54 -11.05 -1.21 0.00 0.00 0.00 62.29
WHEEL (0.00 + 54.29 + 0.00) = 54.29 dBA
Anglel Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
   -90 55 0.24 67.75 -12.07 -1.39 0.00 0.00 0.00 54.29
Segment Leq: 62.93 dBA
Total Leq All Segments: 62.93 dBA
Results segment # 1: CN Halton (night)
LOCOMOTIVE (0.00 + 64.01 + 0.00) = 64.01 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
  -90 55 0.14 76.26 -11.05 -1.21 0.00 0.00 0.00 64.01
WHEEL (0.00 + 56.15 + 0.00) = 56.15 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
   -90 55 0.24 69.61 -12.07 -1.39 0.00 0.00 0.00 56.15
Segment Leq: 64.67 dBA
Total Leg All Segments: 64.67 dBA
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Road data, segment # 1: Guelph St (day/night)
Car traffic volume : 26925/2992 veh/TimePeriod *
Medium truck volume : 1095/122 veh/TimePeriod *
Heavy truck volume : 807/90 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)
* Refers to calculated road volumes based on the following input:
    24 hr Traffic Volume (AADT or SADT): 24275
Percentage of Annual Growth : 2.00
Number of Years of Growth : 14.00
    Medium Truck % of Total Volume : 3.80
Heavy Truck % of Total Volume : 2.80
Day (16 hrs) % of Total Volume : 90.00
Data for Segment # 1: Guelph St (day/night)
Angle1 Angle2 : 35.00 deg
                                                  90.00 deg
wood depth : 0
No of house rows : 0 / 0
Surface
                                                  (No woods.)
                               : 1 (Absolute 186.00 m
Surface
                                                  (Absorptive ground surface)
Receiver source distance
Receiver height : 16.50 m
Topography
                               : 0.00
                                        1 (Flat/gentle slope; no barrier)
Topography
Reference angle
Results segment # 1: Guelph St (day)
Source height = 1.29 \text{ m}
ROAD (0.00 + 50.38 + 0.00) = 50.38 dBA
Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
    35 90 0.22 69.77 0.00 -13.30 -6.09 0.00 0.00 0.00 50.38
Segment Leg: 50.38 dBA
Total Leg All Segments: 50.38 dBA
Results segment # 1: Guelph St (night)
Source height = 1.29 \text{ m}
ROAD (0.00 + 43.86 + 0.00) = 43.86 dBA
Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
    35 90 0.22 63.25 0.00 -13.30 -6.09 0.00 0.00 0.00 43.86
Segment Leg: 43.86 dBA
Total Leq All Segments: 43.86 dBA
TOTAL Leg FROM ALL SOURCES (DAY): 63.16
                              (NIGHT): 64.71
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